

## **INTERIM PROCEDURE FOR TYPE APPROVAL OF 406 MHz BEACONS EQUIPPED WITH LI-ION RECHARGEABLE BATTERIES**

**C/S IP (LIRB) – Revision 4**

**October 2014**

The following procedure shall be used by the Cospas-Sarsat Secretariat for the review of type approval applications for 406 MHz beacons equipped with Li-ion rechargeable batteries. Because of the limited experience available and the limitations that may affect beacons equipped with rechargeable batteries, 406-MHz beacons equipped with Li-ion rechargeable batteries successfully tested in accordance with this Interim Procedure will receive a Letter of Compatibility in lieu of a full Cospas-Sarsat Type-Approval Certificate. All C/S T.007 requirements are applicable for type approval testing of beacons equipped with Li-ion rechargeable batteries, except when otherwise stated in this document.

This procedure only applies to rechargeable batteries where lithium ions move from the anode (negative electrode) to the cathode (positive electrode) during discharge and the reverse direction when undergoing charge and where the anode is made from insertion material (hard carbon, graphite, etc.), the cathode is a metal oxide, and the electrolyte is a lithium salt in an organic solvent.

### **1. DEFINITIONS APPLICABLE TO LITHIUM-ION RECHARGEABLE BATTERIES**

#### **1.1 Beacon Modes**

**1.1.1 Beacon Storage Mode:** No circuits are powered by the primary battery<sup>1</sup>.

**1.1.2 Beacon Stand-By Mode:** The beacon 406-MHz transmitter and other ancillary devices are not activated; automatic internal checks are performed from time to time by the beacon resulting in a current drain from the primary battery.

**1.1.3 Beacon Self-Test Mode:** Some beacon circuits are powered during the self-test of the beacon, which results in specific power drain from the primary battery.

**1.1.4 Beacon Active Mode:** The 406-MHz transmitter is active and/or other ancillary devices powered by the primary battery are active.

#### **1.2 Time Between Recommended Charges (TBRC)**

The time between recommended charges (TBRC) at ambient temperature, for this procedure, is the time recommended by the beacon manufacturer between battery recharges when the beacon is in stand-by mode. The TBRC determined by the manufacturer must take into account the power drain which would result from recommended periodic self-tests during TBRC.

The value of TBRC and corresponding temperature must be clearly marked on the beacon.

TBRC is temperature dependent; the beacon manufacturer shall inform the user, by including an appropriate warning in the user manual, that prolonged storage at high temperature will require recharging the beacon more often than stated.

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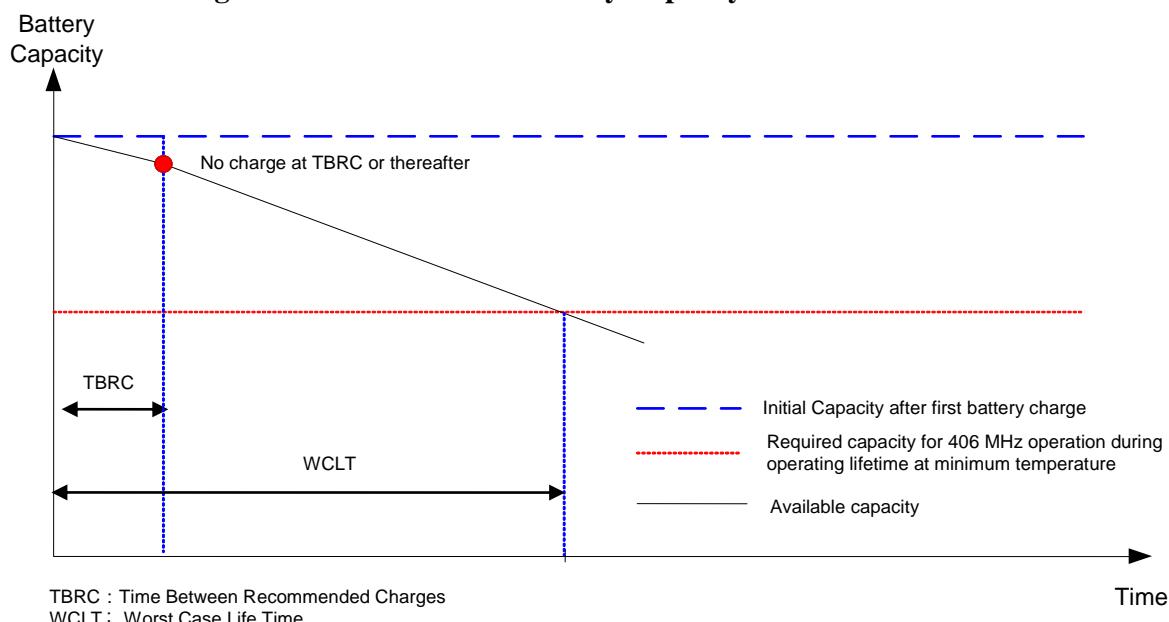
<sup>1</sup> The primary battery is the non-rechargeable or rechargeable battery which is powering the 406-MHz function

### 1.3 New Battery Worst Case Life Time (WCLT)

The term “worst case life time” (WCLT) is used to refer to the worst-case life-time of a new battery. In a worst-case scenario, the user might not recharge<sup>2</sup> the battery after the initial full charge. In this case, the “worst case life time” is the time in beacon stand-by mode when the available capacity remains greater or equal to the capacity required to meet the declared operating life-time at the worst-case operating temperature.

The worst-case life-time is determined by the beacon manufacturer. The WCLT definition assumes no irreversible losses due to beacon storage prior to the first battery charge that initiates the beacon stand-by mode. The definition also assumes that no self-tests are performed during WCLT. If self-tests are recommended by the manufacturer during TBRC, separate from the recharge process, the corresponding current drain would also have to be considered for the determination of WCLT.

**Figure 1: Illustration of Battery Capacity and Worst Case Life Time**



### 1.4 Battery Replacement Period

The Battery Replacement Period is determined by the beacon manufacturer from the sum of the following losses and current drains:

- irreversible capacity loss over the replacement life time and maximum storage time (including the 1.65 safety factor),
- reversible capacity loss during TBRC (including the 1.65 safety factor),
- average current drain resulting from constant operation of the beacon circuits in stand-by mode (including the 1.65 safety factor),

<sup>2</sup> It is assumed that the initial charge of the battery has been done by the user in accordance with the user manual procedure.

d) current drain due to maximum number of self-tests carried out during TBRC as recommended by the beacon manufacturer.

The battery replacement period assumes a maximum storage time of two years (battery storage plus beacon storage) prior to the first full charge of the new battery.

### **1.5 Maximum Storage Time**

Storage time includes the battery storage time prior to its installation in the beacon and the beacon storage time before the first full charge of the battery.

A maximum storage time of two years shall be used for the determination of the battery replacement date and for the calculation of the pre-test battery discharge.

### **1.6 Battery Replacement Date**

The battery replacement date is the date at which the rechargeable battery installed in the beacon must be replaced. The battery replacement date shall be clearly marked on the beacon together with the TBRC. The replacement date is determined by the beacon manufacturer using:

- the date the batch of new batteries was manufactured,
- two years of maximum storage time at the manufacturer's recommended state of charge and prior to the first full charge by the user, and
- the specific battery replacement period determined by the manufacturer for the beacon model.

The battery replacement date is given by the expression:

$$\text{Battery Replacement Date} = \text{Date of Battery Manufacture} + \text{Two Years Storage} + \text{Battery Replacement Period}$$

On the battery replacement date, the beacon shall be capable of supporting continuous operation for the duration of the declared lifetime.

## **2. PROCEDURES FOR TESTING BEACONS WITH LITHIUM-ION RECHARGEABLE BATTERIES**

### **2.1 General Requirements**

All C/S T.007 requirements are applicable for type-approval testing of beacons equipped with Li-ion rechargeable batteries, except when otherwise stated in this document.

### **2.2 Test Conditions**

In addition to provisions of section 4.4 of document C/S T.007, and at the discretion of the test authority, the manufacturer may be required to replace or recharge the LIRBs between tests. However, no other modifications to the beacon will be allowed during the test period without a full re-test.

## 2.3 Technical Data

In addition to the technical data submitted to the Cospas-Sarsat Secretariat, listed in section 5 of document C/S T.007, the beacon manufacturer shall submit supplementary technical information related to the LIRB, in accordance with Appendices A and B of Attachment A of this document.

## 2.4 Changes to Type-Approved Beacons

The manufacturer must advise the Cospas-Sarsat Secretariat (see C/S T.007 Annex H) of any changes to the design or production of the beacon, LIRB or battery charger for beacons equipped with Li-ion rechargeable batteries.

## 2.5 Operating Lifetime at Minimum Temperature

In addition to the requirements described in section A.2.5 of document C/S T.007, calculation of the pre-test battery discharge shall account for the following factors:

- i. the reversible and irreversible losses<sup>3</sup> of battery capacity;
- ii. the battery capacity loss due to constant operation of the circuits powered from the LIRB of a beacon in stand-by mode, over the time between recommended charges (TBRC) ;
- iii. the recommended number of self-tests and, when the function is included, the maximum number and maximum duration of GNSS self-tests, as specified by the beacon manufacturer and allowed by the beacon design, over the battery replacement period;
- iv. the worst-case depletion in battery power due to current draw that cannot be replicated during the lifetime test, for example, to account for a difference between the actual output power setting of the test unit homer transmitter and the maximum output power of the homer transmitter, as declared by the beacon manufacturer in Annex G;
- v. a correction coefficient of 1.65 shall be applied to item (i) to account for differences between battery to battery and the possibility of not recharging the battery at the required time.
- vi. a correction coefficient of 1.65 shall be applied to item (ii), (iii) and (iv) to account for differences from battery to battery, beacon to beacon and the possibility of exceeding the battery replacement time.

The pre-test battery discharge calculations shall be included in the test facility report in the format of Table A-C.1.

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<sup>3</sup> The terms are defined in section 3.1.

## 2.6 Self-Test Mode

For beacons using LIRBs, the battery status should be tested during the self-test. If the battery is not in “normal battery mode” as defined in section 3.1, the self-test result should indicate “Failure”.

# 3. PROCEDURES FOR EVALUATION OF LI-ION RECHARGEABLE BATTERIES PERFORMANCE

## 3.1 Definitions

### 3.1.1 Normal Battery Mode

The beacon manufacturer shall state the time between recommended charges (TBRC). The beacon shall automatically check the battery condition at defined intervals ( $T_{\text{wake-up}}$ ), which shall not be longer than one fourth of TBRC. At the end of each  $T_{\text{wake-up}}$  interval, the beacon shall check the time since the last charge and the battery condition, and:

- If the time since the last charge is less than TBRC and if the battery condition is good, the battery is considered to be in “Normal Battery Mode” and the beacon may go back to standby mode until the end of the next  $T_{\text{wake-up}}$  interval.
- If the above conditions are not fulfilled, the user shall be warned by audio and/or light indication that the battery must be recharged (see section 3.2 for indication of LIRB-charge status).

### 3.1.2 Irreversible Capacity Loss

The irreversible capacity loss is the loss of the battery capacity which cannot be recovered by subsequent recharges of the battery. There are two components to the total irreversible capacity loss:

- (i) during battery and beacon storage, and
- (ii) during the battery replacement period while the beacon is in standby mode.

### 3.1.3 Reversible Capacity Loss

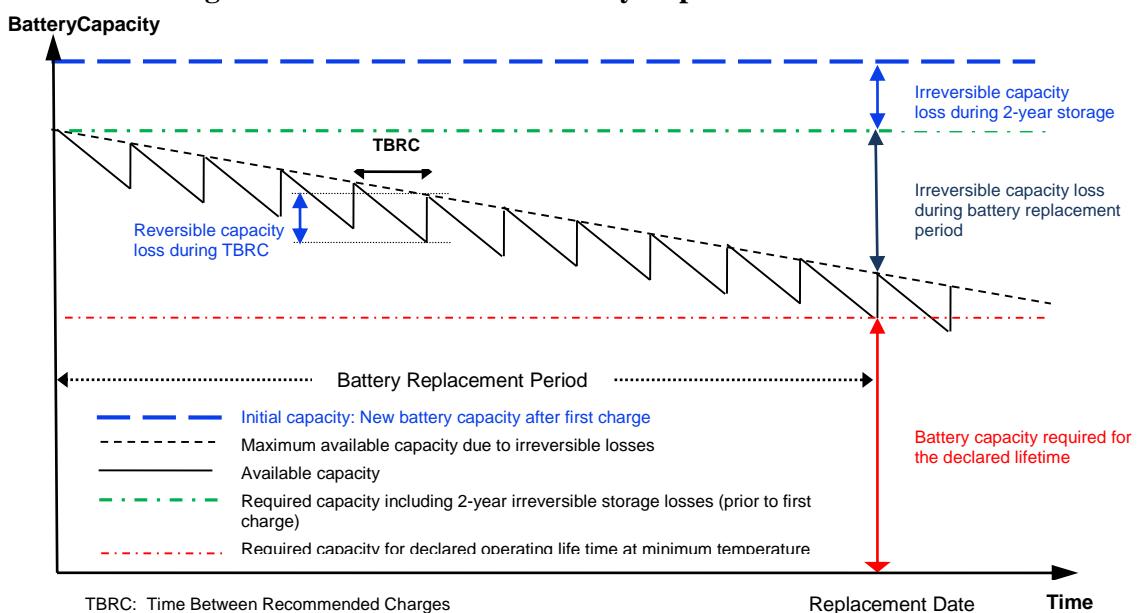
The reversible capacity loss is the loss of the battery capacity which can be recovered by subsequent recharges of the battery.

### 3.1.4 Determination of the Battery Replacement Period

Figure 2 illustrates the determination of the battery replacement period. The diagram of available battery capacity assumes that, initially, the new battery installed in the beacon is fully charged and is not affected by any irreversible storage loss. To take irreversible storage losses into consideration, the battery capacity required to meet the specified performance during the declared operating life time at minimum temperature is augmented by the irreversible storage loss assuming a maximum two year storage time (battery storage and beacon storage mode).

The operating life time at minimum temperature performance of the beacon on the battery replacement date shall be verified using the procedure described in section A.2.3 of document C/S T.007.

**Figure 2: Determination of Battery Replacement Period**



### 3.1.5 New Battery Worst Case Life Time (WCLT)

The term “worst case life time” (WCLT) is used to refer to the worst-case life-time of a new battery. In a worst-case configuration, the user might forget to recharge the beacon battery. The WCLT is the time in beacon stand-by mode when the available capacity remains greater or equal to the capacity required to meet the declared operating life time at the worst-case temperature. The WCLT shall be at least 1 month greater than the beacon manufacturer-declared TBRC.

The beacon manufacturer shall state the WCLT value in the type approval application and indicate the WCLT value in the user manual.

## 3.2 Battery Charge Indication

Beacons using rechargeable batteries shall provide a clear indication of when the battery should be recharged. This indication should be provided either by visual (e.g., LED display) and/or by audio indicator (e.g., buzzer). Beacon manufacturers may choose to indicate:

- either that the battery is in “normal battery mode” (for example, by activating a green LED); or
- that the battery is no longer in “normal battery mode” (for example, by flashing a red LED).

Indication of the beacon battery charge shall be described in the user manual and shall be verified by the test facility during TA testing.

### 3.3 Measurement of Remaining Battery Capacity at the Replacement Date

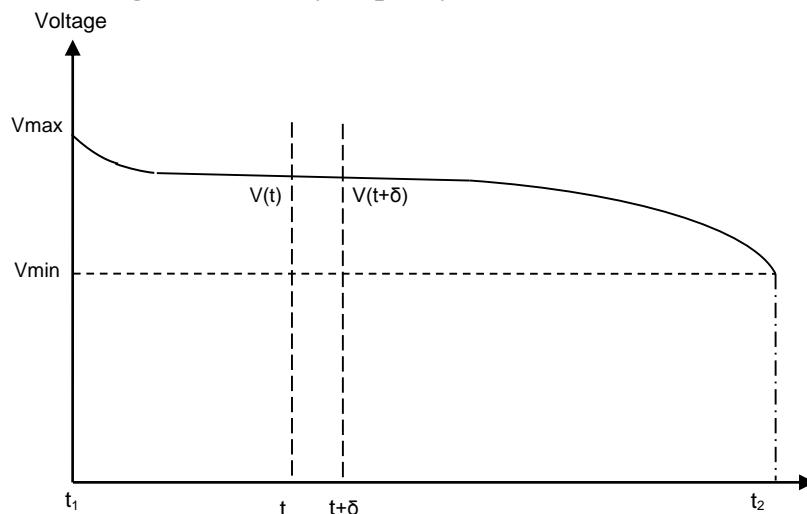
#### 3.3.1 Battery Capacity Measurement

The capacity of the battery can be defined as  $C = \int_{t_1}^{t_2} I(t) \cdot dt$

The measurement of the battery capacity shall be made using the following procedure:

- a complete charge process is made on the battery (at time  $t_1$  in Figure 3 the battery is fully charged);
- a discharge of the battery is made using a well known resistor  $R_{\text{discharge}}$  until the battery is fully discharged, the voltage goes down to zero<sup>4</sup> (at time  $t_2$  in Figure 3 the battery is “empty”); and
- the voltage is monitored every  $\delta t$ .

**Figure 3: Battery Capacity Measurement Procedure**



The capacity is calculated as follows:

$$C = \int_{\text{Fully-charged}}^{\text{Empty Battery}} I(t) \cdot dt = \frac{1}{R_{\text{discharge}}} \sum_{t_1}^{t_2} \left( \frac{V(t + \delta t) + V(t)}{2} \cdot \delta t \right)$$

$R_{\text{discharge}}$  is chosen in order to provide an equivalent discharge current equal to the maximum charge current of the charger when the battery is at its maximum (i.e., fully charged at  $V_{\text{max}}$  in Figure 3 above).<sup>5</sup>

The value of the resistor  $R_{\text{discharge}}$  has to be known to an accuracy better than 1%.

<sup>4</sup> In most cases, the battery is not really fully discharged, but an internal protection switch (inside PCM: protection circuit modules) is activated when the voltage is below  $V_{\text{min}}$  (usually 2,5V) to avoid deep discharge of the battery, which is not recommended for Li-Ion technology. This protection is usually deactivated by a charge process. This PCM is also used to protect against overcharge and short-circuits.

<sup>5</sup> For example, most Li-Ion cells are to be charged at 4.2V. So if the battery is 2000mAH, and if the maximum charge current is  $C/5=2000/5=400\text{mA}$ ,  $R$  is  $4.2/0.4=10.5\text{ Ohms}$ .

### 3.3.2 Measurement of Reversible Capacity Loss at Room Temperature

The measurement of Reversible Capacity Loss shall be performed by the beacon manufacturer

In this section, when a battery is recharged, the charger to be used shall be as described in section 3.6 of this document.

The measurement is performed using a batch of 10 batteries. The batteries shall initially be fully charged ( $V_{charge\_final} = V_{max}$ ). The first capacity measurement shall be made at room temperature at time  $t_0$  on each battery of the batch (as detailed in section 3.3.1 of this document). The average  $C_{0\_mean}$  is then calculated.

**Figure 4: Time Line for Capacity Loss Measurements during TBRC**



The batteries are then fully recharged, disconnected and left unconnected during TBRC.

At  $t_0+TBRC$ , a voltage measurement is made on each battery to provide the battery voltage after TBRC. The average  $V_{partial\_discharge\_mean}$  is calculated<sup>6</sup>.

A second capacity<sup>7</sup> measurement is made on each battery at room temperature at  $t_0+TBRC$ . The average  $C_{1\_mean\_TBRC}$  is calculated.

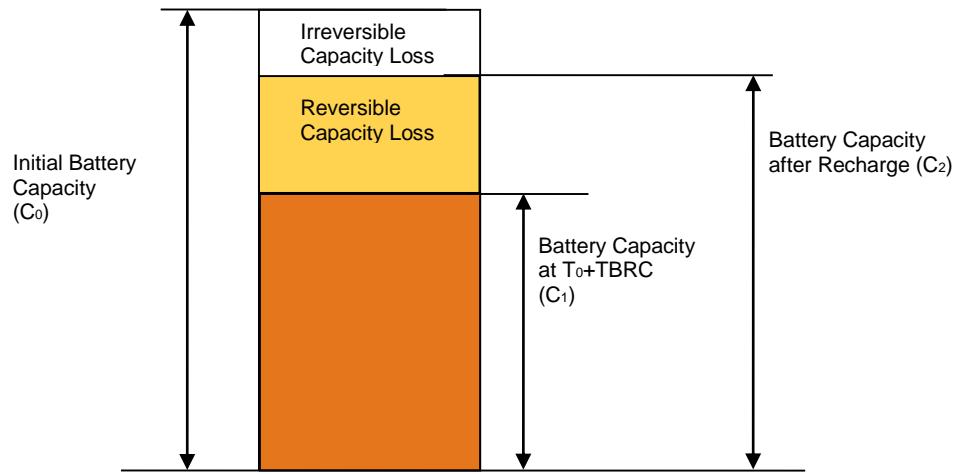
Based on the dispersion of the individual measurements of  $C_{reversible\_losses\_during\_TBRC}$ , the manufacturer determines a  $C_{maximum\_reversible\_losses\_during\_TBRC}$ .

Based on the dispersion of the individual measurements of  $C_{irreversible\_losses\_during\_TBRC}$ , the manufacturer determines a  $C_{maximum\_irreversible\_losses\_during\_TBRC}$ .

After the capacity measurement at  $t_0+TBRC$ , a complete recharge of all batteries is performed. A third capacity measurement is made on each battery at room temperature and the average  $C_{2\_mean\_TBRC}$  is calculated.

<sup>6</sup> This information is important for taking into account the impact of multiple charge-discharge processes on irreversible capacity losses as described in section 3.3.3 (ii) of this document.

<sup>7</sup> The second capacity measurement is made before performing any recharge.

**Figure 5: Illustration of Battery Capacity and Losses**

The reversible battery capacity loss during TBRC (after the first recharge) is then:

$$C_{\text{reversible\_loss}} = C_{2\text{-mean\_TBRC}} - C_{1\text{-mean\_TBRC}}$$

The irreversible battery capacity loss during TBRC is also calculated as follows:

$$C_{\text{irreversible\_losses\_during\_TBRC}} = C_{0\text{-mean\_TBRC}} - C_{2\text{-mean\_TBRC}}.$$

### 3.3.3 Evaluation of Irreversible Capacity Losses: Accelerated Aging

This evaluation is performed by the beacon manufacturer.

The Arrhenius equation states that the dependence of the rate constant  $k$  of chemical reactions to the temperature  $T$  (in Kelvin) and activation energy  $E_a$  is given by the following equation:

$$\lambda = A \cdot e^{-\frac{E_a}{RT}}$$

Where:

- $\lambda$  : rate of capacity fade
- $A$  : pre exponential factor
- $E_a$  : activation energy as measured in section 3.9 of this document (in  $\text{J}\cdot\text{mol}^{-1}$ )
- $R$  :  $8.31 \text{ J}\cdot\text{mol}^{-1}\cdot\text{K}^{-1}$
- $T$  : temperature (in Kelvin)

In order to simulate the ageing of batteries within a reasonable test time, the batteries are placed at a higher temperature in a climatic chamber. The equivalent ageing of the capacity of the battery follows the Arrhenius law whereby an accelerated ageing of the battery can be achieved.

The activation energy is dependent upon the selected battery chemistry and cell construction (i.e., the chosen Anode-Cathode-Electrolyte chemistry), the beacon manufacturer has to measure this parameter as described in section 3.9 of this document.

The accelerated ageing factor is then calculated according to the expression:

$$\frac{t_1}{t_2} = e^{\frac{E_a}{R} \left( \frac{1}{T_1} - \frac{1}{T_2} \right)} \text{ with:}$$

- $t_1$  : time of the test at ambient temperature
- $T_1$  : ambient temperature 293°K (i.e. equal to 20°C±1°C)
- $t_2$  : time of the test at elevated temperature ( $t_1 > t_2$ )
- $T_2$  : climatic chamber temperature in °K ( $\pm 1^{\circ}\text{K}$ ) ( $T_2 > T_1$ )

The selected test temperature shall correspond to a test period greater than 6 months and shall not exceed 55°C so as to avoid a distortion of ageing results.

(i) Estimation of Irreversible Capacity Loss during Storage

This test is performed by the beacon manufacturer using a batch of 10 new batteries. These batteries are to be supplied by the battery manufacturer as they will be supplied in production (i.e., most of the time they will not be fully charged).

At time  $t_0$ ,  $C_0$  capacity measurements are made at room temperature on a set of five batteries using the procedure described in section 3.3.1 of this document. These five batteries are not used for the remainder of the test. The average  $C_{0\_mean}$  is calculated from the measurements obtained for these five batteries.

The other set of five batteries is left unconnected and not charged. The batteries are placed in a climatic chamber at the selected temperature during the test period equivalent to the maximum storage period at ambient temperature, as described above. The batteries are then removed from the climatic chamber. A complete charge is performed on these batteries and capacity measurements are made on all five batteries at room temperature to provide the average  $C_{2\_mean\_storage}$ .

The irreversible capacity loss due to storage is calculated as follows:

$$C_{\text{irreversible\_loss\_in\_storage}} = C_{0\_mean} - C_{2\_mean\_storage}$$

(ii) Estimation of Irreversible Capacity Loss During Beacon Standby Mode

This test is performed by the beacon manufacturer using a batch of 10 new batteries, as supplied by the battery manufacturer.

At time  $t_0$ ,  $C_0$  capacity measurements are made at room temperature on a set of five batteries using the procedure described in section 3.3.1 of this document. These five batteries are not used for the remainder of the test. The average  $C_{0\_mean}$  is calculated from the measurements obtained for these five batteries.

The other set of five batteries is charged and placed in a climatic chamber at the selected temperature for the test period equivalent to the battery replacement life time at ambient temperature, as described above.

At time  $t_0 + \text{test period}$ , the five batteries are taken out from the climatic chamber. To take into account the aging linked to the repetitive charge-discharge process,  $N$  successive charge-discharge cycles are performed as follows:

The charge process is made using the charger as described in section 3.6 of this document and the discharge process is made from  $V_{charge\_final}$ <sup>8</sup> to  $V_{partial\_discharge\_mean}$  in  $R_{discharge}$ <sup>9</sup>. This step is repeated N times on all five batteries, with N defined as the ratio: Battery Replacement Period / TBRC, rounded down to the nearest integer.

Finally a charge process is applied on all five batteries and new capacity measurements  $C_2$  are made. The average  $C_{2\_mean\_Standby}$  is calculated.

The irreversible capacity loss in standby mode during the battery replacement period, including the partial discharge/recharge cycles applied in beacon standby mode, is calculated as follows:

$$C_{irreversible\_loss\_in\_Stand-by\_mode} = C_{0\_mean} - C_{2\_mean\_Standby}$$

(iii) Estimation of Total Irreversible Losses

The total irreversible losses, which include storage loss and loss during normal mode, are:

$$C_{irreversible\_losses} = C_{irreversible\_loss\_in\_storage} + C_{irreversible\_loss\_in\_Standby\_mode}$$

An additional safety factor of 1.65 is to be applied to this value when performing the operating life time at minimum temperature test per section A.2.3 of document C/S T.007.

### 3.4 Verification of Reversible and Irreversible Capacity Losses

In order to partially verify the results provided by the beacon manufacturer, the following measurements shall be performed by a Cospas-Sarsat accepted test facility.

The measurements are performed on a batch of 5 batteries. The batteries are initially fully charged. At time  $t_0$ , the first capacity measurement is made at room temperature on each battery of the batch. The average  $C_{0\_mean\_lab}$  is calculated.

The batteries are recharged, disconnected and left unconnected during TBRC.

At time  $t_0+TBRC$ , a second capacity measurement is made at room temperature. The  $C_{1i}$  capacity is measured for each battery. After this capacity measurement, the batteries are recharged. A third capacity measurement is then made at room temperature. The  $C_{2i}$  capacity is measured for each battery.

The following battery capacity losses are derived from the above measurements:

- (i) Reversible loss between successive charges =  $C_{2i}-C_{1i}$   
Each value has to be smaller than  $C_{maximum\_reversible\_losses\_during\_TBRC}$  provided by the beacon manufacturer as described in section 3.3.2 of this document,
- (ii) Irreversible loss between successive charges =  $C_{0i}-C_{2i}$

<sup>8</sup> See definitions in 3.6.2 of this document and Figure 7.  $V_{charge\_final}$  = battery voltage at end-of-charge.

<sup>9</sup> See definitions in section 3.3.2 of this document.

Each value has to be smaller than  $C_{\text{maximum\_irreversible\_losses\_during\_TBRC}}$  provided by the beacon manufacturer as described in section 3.3.2 of this document.

If the values of reversible and irreversible battery capacity losses during TBRC, derived from (i) and (ii) above, are different from the values provided by the beacon manufacturer, the highest values of each parameter shall be used by the test facility for calculation of pre-test battery discharge.

### 3.5 Verification of Worst Case Life Time

This test is performed by the beacon manufacturer using two complete beacons equipped with new batteries.

At time  $t_0$ , the batteries of the beacons are charged. After the charge, the beacons in stand-by mode are placed in a climatic chamber set to a specific temperature ( $T_{\text{wclt}}$ ) for a duration equivalent to the declared Worst Case Life Time (WCLT) at ambient temperature. As described in section 3.3.3 of this document, the accelerated ageing factor  $\lambda_{\text{wclt}}$  is a function of  $E_a$  and  $T_{\text{wclt}}$ :

$$\lambda_{\text{wclt}} = e^{\frac{E_a}{R} \left( \frac{1}{T_1} - \frac{1}{T_{\text{wclt}}} \right)}$$

The equivalent WCLT duration is the WCLT divided by the factor  $\lambda_{\text{wclt}}$ .

At the end of the test period the beacons are removed and kept at ambient temperature for at least 2 hours. Then the beacons are put in a climatic chamber at their minimum operating temperature and, after at least 2 hours of soaking, the beacons are turned on. An operating life time test at minimum temperature is then carried out on both beacons as described in document C/S T.007 section A.2.3, but without any further pre-conditioning of the battery. If the operating life-time test is successful for both beacons (i.e., the beacons meet Cospas-Sarsat requirements for the declared operating lifetime at minimum temperature), the declared worst-case life-time is deemed to be confirmed by the test.

The results of WCLT evaluation and the results of lifetime tests shall be submitted by the beacon manufacturer as part of the application package.

### 3.6 Battery Charger

#### 3.6.1 Charger Information

The electric diagram of the charger and description of the charger working cycle shall be provided by a beacon manufacturer as part of the application package.

For CCCV (Constant Current and Constant Voltage) charge, the following information shall be provided:

- a) charge current during constant current phase (this value could be provided as a function of the battery capacity<sup>10</sup>),

<sup>10</sup> For example, for a 2000 mAH battery, a charge at C/5 would mean a charge current of 2000/5=400 mA.

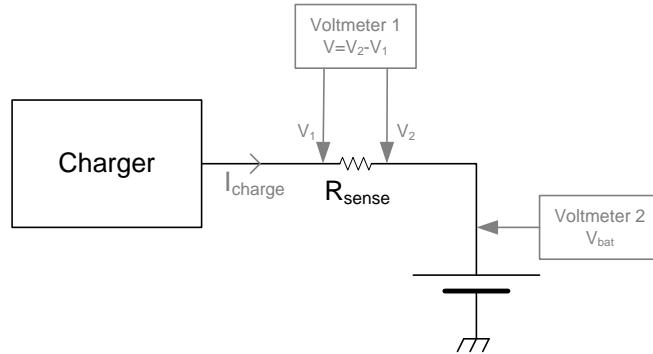
- b) charge voltage and tolerance during constant voltage phase (for example 4.2 V for most Li-ion cells),
- c) current limit below which the charging process is ended,
- d) estimated time to fully recharge a battery,
- e) confirmation that the charger is compliant with national safety/EMC requirements,
- f) description of the beacon battery charger, its working cycle and indicators.

### 3.6.2 Charger Test Procedure for CCCV Charge Process

These measurements may be performed by a beacon manufacturer, and shall be verified by an accepted test facility.

- a) Test Set-Up

**Figure 6: Diagram of Beacon Charger Test Set-Up**



Two voltmeters are necessary, one for differential measurement (image of the charge current), the other for monitoring the voltage of the battery.

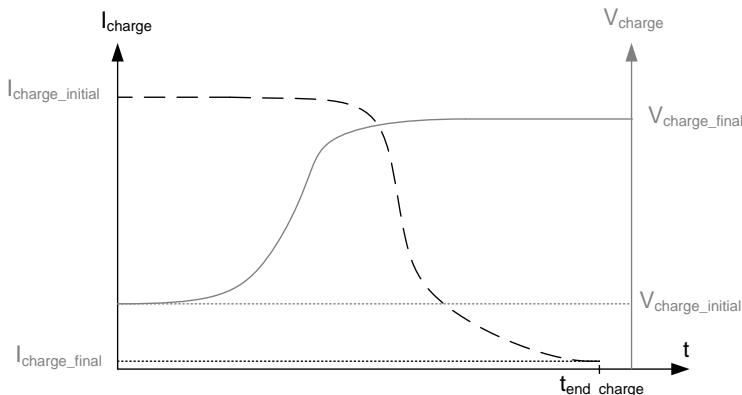
$$I_{charge} = \frac{V_2 - V_1}{R_{sense}}$$

$R_{sense}=0.1$  Ohms (with accuracy lower or equal to 1%)

- b) Test Procedure and Test Result

In a first step, the battery has to be fully discharged in a defined resistor as described in section 3.3.1 of this document. The battery is then charged and  $I_{charge}$  and  $V_{charge}$  are monitored.

At least 50 values ( $I_{charge}$  and  $V_{charge}$ ) are to be provided and the time between two successive measurements shall not be longer than 1 minute.

**Figure 7: Voltage and Current Intensity Measurements during Battery Charge**

The charge applied to the battery shall then be calculated in mA-hrs. The charge applied shall be equal or greater than the battery capacity measured in section 3.3.1 of this document.

The test facility shall verify that distinct indication of an on-going charge and an end of charge are provided.

### 3.7 Verification of the Battery Charge Status during Self-Test

During the self-test, the battery mode should be tested. If the battery is not in normal mode, the self-test result shall indicate "Failure".

### 3.8 Data to be Provided by Beacon Manufacturers

All information specific to the use of rechargeable batteries is documented in Attachment A to this document.

### 3.9 Measurement Method of the Activation Energy

The Arrhenius law applied to batteries is  $C_{residual} = C_0 \cdot e^{-\lambda t}$  with  $\lambda = \lambda_0 \cdot e^{-\frac{E_a}{RT}}$

Measurements are made:

- at 4 different temperatures,
- during 3 different time periods, and
- using 5 batteries for each measurement (in time and temperature).

A total of 60 batteries are needed for the test.

#### (i) Definition of the different temperatures

The four recommended temperatures<sup>11</sup> are:

- $T_1 = 20^\circ\text{C}$
- $T_2 = 30.8^\circ\text{C}$
- $T_3 = 42.4^\circ\text{C}$
- $T_4 = 55^\circ\text{C}$

<sup>11</sup> T2 & T3 are chosen to have 3 regular steps on the curve in 1/T (T in °K) between  $T_1$  &  $T_4$

(ii) Definition of the different measurement times

In order to define the measurement steps, a first “estimation” of the activation energy is needed. The first estimated “proposed value” is  $E_a = 40 \text{ kJ.mol}^{-1}$ . The associated accelerated ageing factor is:

$$\frac{t_1}{t_2} = e^{\frac{E_a}{R} \left( \frac{1}{T_1} - \frac{1}{T_4} \right)} = e^{\frac{40 \cdot 10^3}{8.31} \left( \frac{1}{273+20} - \frac{1}{273+55} \right)} = 5.7$$

The duration of the test is then defined by:

$$t_{Ea\_test} = \frac{\text{period equivalent to the replacement period}}{5.7}$$

If the calculated value is below 6 months, the test is then defined to last 6 months.

The three recommended time periods are:

- $\tau_1 = t_{Ea\_test} \cdot 1/3$
- $\tau_2 = t_{Ea\_test} \cdot 2/3$
- $\tau_3 = t_{Ea\_test}$

(iii)  $E_a$  measurement

At the beginning of the test,

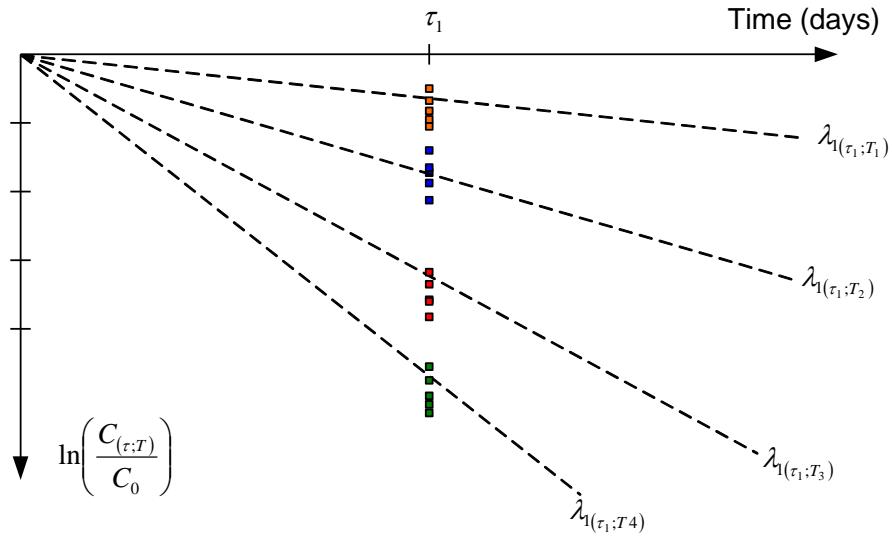
- 15 batteries are placed in a climatic chamber at  $T_1=20^\circ\text{C}$
- 15 batteries are placed in a climatic chamber at  $T_2=30.8^\circ\text{C}$
- 15 batteries are placed in a climatic chamber at  $T_3=42.4^\circ\text{C}$
- 15 batteries are placed in a climatic chamber at  $T_4=55^\circ\text{C}$

After a period  $\tau_1 = t_{Ea\_test} \cdot 1/3$ , a set of 5 batteries is extracted from each climatic chamber and their remaining capacity is measured.

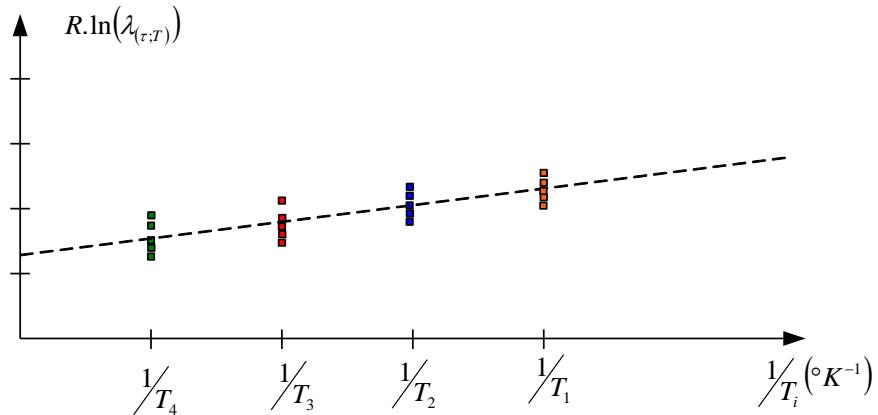
- For the 1<sup>st</sup> group stored at  $T_1$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_1; T_1); C_{\text{residual\_2}}(\tau_1; T_1); C_{\text{residual\_3}}(\tau_1; T_1); C_{\text{residual\_4}}(\tau_1; T_1); C_{\text{residual\_5}}(\tau_1; T_1)$ .
- For the 2<sup>nd</sup> group stored at  $T_2$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_1; T_2); C_{\text{residual\_2}}(\tau_1; T_2); C_{\text{residual\_3}}(\tau_1; T_2); C_{\text{residual\_4}}(\tau_1; T_2); C_{\text{residual\_5}}(\tau_1; T_2)$ .
- For the 3<sup>rd</sup> group stored at  $T_3$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_1; T_3); C_{\text{residual\_2}}(\tau_1; T_3); C_{\text{residual\_3}}(\tau_1; T_3); C_{\text{residual\_4}}(\tau_1; T_3); C_{\text{residual\_5}}(\tau_1; T_3)$ .
- For the 4<sup>th</sup> group stored at  $T_4$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_1; T_4); C_{\text{residual\_2}}(\tau_1; T_4); C_{\text{residual\_3}}(\tau_1; T_4); C_{\text{residual\_4}}(\tau_1; T_4); C_{\text{residual\_5}}(\tau_1; T_4)$ .

According to:  $C_{\text{residual}} = C_0 \cdot e^{-\lambda t}, \quad \ln\left(\frac{C_{\text{residual}}}{C_0}\right) = -\lambda t$

The measured values are incorporated in the graph below (Figure 8).

**Figure 8: Capacity Versus Time at  $\tau_1$** 

**Note:** In Figure 8, only 1 of the 5 lines corresponding to the 5 measured values are depicted. For each measurement, 5 batteries are used as defined in the 1<sup>st</sup> paragraph of section 3.9 of this document. The slopes of the lines in Figure 8 provide different values of  $\lambda_k(\tau_1; T_i)$ , which are depicted in Figure 9. At  $\tau_1$ , 20 values are to be reported on Figure 8, corresponding to 20 data point on Figure 9 (i.e. 5 at  $1/T_4$ , 5 at  $1/T_3$ , 5 at  $1/T_2$  and 5 at  $1/T_1$ ).

**Figure 9: Accelerated Ageing Factor Versus Temperature at  $\tau_1$** 

The measured activation energy ( $E_{a\_meas}$ ) is the slope of the best fit straight line shown in Figure 9. The accelerated ageing factor shall be recalculated according to the expression:

$$\lambda = e^{\frac{E_{a\_meas}}{R} \left( \frac{1}{T_1} - \frac{1}{T_4} \right)}$$

The duration of the test is then recalculated as:

$$t_{Ea\_test} = \frac{\text{period equivalent to the replacement life time}}{\lambda}$$

At time  $\tau_2 = 2/3 \cdot t_{Ea\_test}$  a set of 5 batteries is extracted from each climatic chamber and their remaining capacity is measured.

- For the 1<sup>st</sup> group stored at  $T_1$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_2; T_1); C_{\text{residual\_2}}(\tau_2; T_1); C_{\text{residual\_3}}(\tau_2; T_1); C_{\text{residual\_4}}(\tau_2; T_1); C_{\text{residual\_5}}(\tau_2; T_1)$ .
- For the 2<sup>nd</sup> group stored at  $T_2$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_2; T_2); C_{\text{residual\_2}}(\tau_2; T_2); C_{\text{residual\_3}}(\tau_2; T_2); C_{\text{residual\_4}}(\tau_2; T_2); C_{\text{residual\_5}}(\tau_2; T_2)$ .
- For the 3<sup>rd</sup> group stored at  $T_3$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_2; T_3); C_{\text{residual\_2}}(\tau_2; T_3); C_{\text{residual\_3}}(\tau_2; T_3); C_{\text{residual\_4}}(\tau_2; T_3); C_{\text{residual\_5}}(\tau_2; T_3)$ .
- For the 4<sup>th</sup> group stored at  $T_4$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_2; T_4); C_{\text{residual\_2}}(\tau_2; T_4); C_{\text{residual\_3}}(\tau_2; T_4); C_{\text{residual\_4}}(\tau_2; T_4); C_{\text{residual\_5}}(\tau_2; T_4)$ .

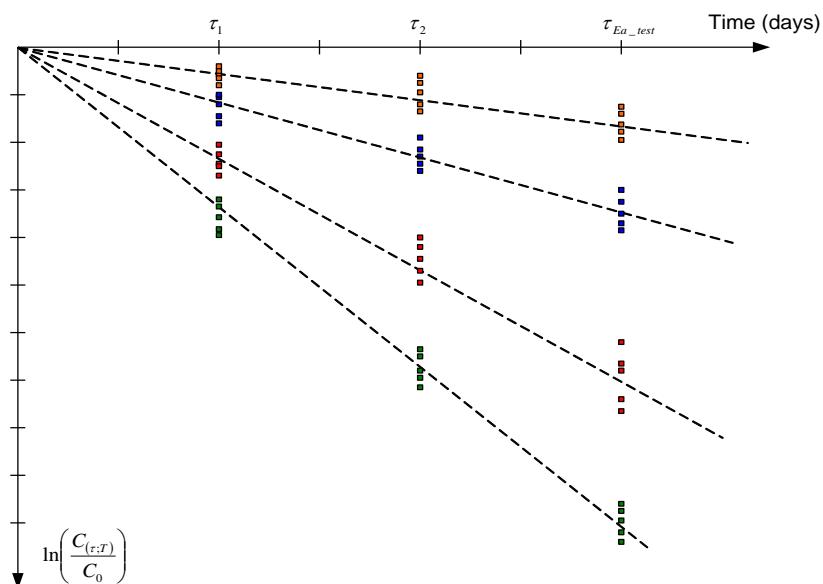
Then the plots “capacity versus time” and “accelerated ageing factor versus temperature” are updated and the duration of the test ( $t_{Ea\_test}$ ) is recalculated.

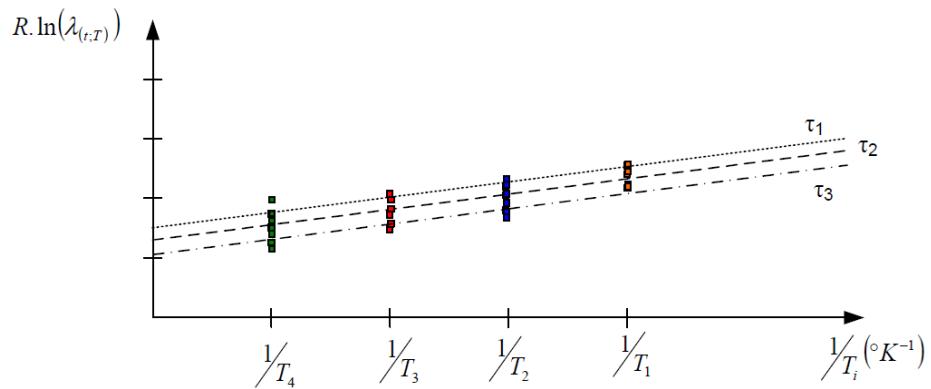
At time  $\tau_3 = t_{Ea\_test}$  the last set of 5 batteries is extracted from each climatic chamber and their remaining capacity is measured.

- For the 1<sup>st</sup> group stored at  $T_1$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_3; T_1); C_{\text{residual\_2}}(\tau_3; T_1); C_{\text{residual\_3}}(\tau_3; T_1); C_{\text{residual\_4}}(\tau_3; T_1); C_{\text{residual\_5}}(\tau_3; T_1)$ .
- For the 2<sup>nd</sup> group stored at  $T_2$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_3; T_2); C_{\text{residual\_2}}(\tau_3; T_2); C_{\text{residual\_3}}(\tau_3; T_2); C_{\text{residual\_4}}(\tau_3; T_2); C_{\text{residual\_5}}(\tau_3; T_2)$ .
- For the 3<sup>rd</sup> group stored at  $T_3$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_3; T_3); C_{\text{residual\_2}}(\tau_3; T_3); C_{\text{residual\_3}}(\tau_3; T_3); C_{\text{residual\_4}}(\tau_3; T_3); C_{\text{residual\_5}}(\tau_3; T_3)$ .
- For the 4<sup>th</sup> group stored at  $T_4$ , 5 capacities are measured:  
 $C_{\text{residual\_1}}(\tau_3; T_4); C_{\text{residual\_2}}(\tau_3; T_4); C_{\text{residual\_3}}(\tau_3; T_4); C_{\text{residual\_4}}(\tau_3; T_4); C_{\text{residual\_5}}(\tau_3; T_4)$ .

The plots “capacity versus time” (Figure 10) and “accelerated factor versus temperature” (Figure 11) are updated.

**Figure 10: Capacity Versus Time at  $\tau_3$**



**Figure 11: Accelerated Ageing Factor Versus temperature at  $\tau_3$** 

The final value of the applicable activation energy (Ea) for the selected technology is the third slope of the best straight fit line shown in Figure 11<sup>12</sup>.

<sup>12</sup> At  $\tau_3$ , 60 values should be reported in Figure 10, hence 60 slopes corresponding to 60 points in Figure 11 (i.e. 15 at  $1/T_4$ , 15 at  $1/T_3$ , 15 at  $1/T_2$  and 15 at  $1/T_1$ ). The activation energy is calculated using value from the individual storage period. Figure 11 presents three slopes for each storage period.

**ATTACHMENT A****APPENDIX A TO ATTACHMENT A****Supplementary Application Form for Beacons Equipped with LIRBs**

| <b>Characteristic</b>   | <b>Specification</b>   |
|---|--|
| Battery chemistry   |  |
| Battery cell model name, size and number of cells   |  |
| Battery cell manufacturer   |  |
| Battery pack manufacturer and part number   |  |
| Initial capacity of new battery after first charge  | _____ mAh  |
| Required capacity to meet the operating life time at minimum temperature                      | _____ mAh  |
| Battery replacement period  | _____ Years  |
| Charge indication   | <input type="checkbox"/> Visual / <input type="checkbox"/> Audio<br><input type="checkbox"/> In Normal Mode / <input type="checkbox"/> Not in Normal mode<br><input type="checkbox"/> Charge Ongoing<br><input type="checkbox"/> Charge Complete<br>Type : |
| Time Between Recommended Charges at ambient temperature (TBRC)                                | _____ Months   |
| T <sub>wake-up</sub> (wake-up period to check battery)  | _____ Days   |
| R <sub>discharge</sub> (resistor for discharge process)                                       | _____ Ω  |
| Reversible losses between TBRC:<br>C <sub>maximum_reversible_losses_during_TBRC</sub>         | _____ %  |
| Voltage drop after TBRC: V <sub>partial_discharge_mean</sub>                                  | _____ V  |
| Irreversible losses during TBRC:<br>C <sub>maximum_irreversible_losses_during_TBRC</sub>      | _____ %  |
| Activation Energy E <sub>a</sub>  | _____ J.mol <sup>-1</sup>  |
| Test temperature (if applicable) for measurement of irreversible capacity loss during storage | _____ °C -   |
| Worst Case Life Time (WCLT)   | _____ Months - _____ Years   |

| Characteristic   | Specification |
|--|---------------|
| Irreversible losses in two-year storage: $C_{irreversible\_loss\_in\_storage}$                                   | _____ %       |
| Test temperature (if applicable) for measurement of irreversible capacity loss in standby mode                   | _____ °C      |
| Irreversible losses in standby mode over battery replacement period: $C_{irreversible\_loss\_in\_standby\_mode}$ | _____ %       |
| Measured operating life time in Worst Case Life Time configuration   | _____ Hours   |
| <b>Battery Charger</b>   |               |
| $I_{charge\_initial}$  | _____ mA      |
| $I_{charge\_final}$  | _____ mA      |
| $V_{charge\_initial}$  | _____ V       |
| $V_{charge\_final}$  | _____ V       |
| Charge time : $t_{end\_charge}$  | _____ Mn      |
| Charge capacity  | _____ mAh     |
| Oscillator type (e.g. OCXO, MCXO, TCXO) ...  |               |

[...]

| Characteristic  | Specification  |                              |
|---|----------------|------------------------------|
| <b>Self-Test Mode Characteristics:</b>  | Self-Test Mode | Optional GNSS Self-Test Mode |
| [...]   |                |                              |
| - Maximum number of GNSS Self-Tests (beacons with internal navigation devices only)                     | N/A            |                              |
| - Self-test automatically activated after each charge process (for beacon using rechargeable batteries) |                |                              |

**APPENDIX B TO ATTACHMENT A****Table A-B.1: Check-List of Technical Information**

| <b>Tick (✓) to indicate submission of items</b> | <b>Applicable Requirements</b> | <b>Description of technical information item</b>                                  | <b>File name, title of document, page, section, where the item is located</b> |
|---|--------------------------------|---|---|
|   | C/S IP(LIRB) Appendix A        | Supplementary Application Form for Beacons equipped with LIRBs                    |   |
|   | C/S T.007, 5(g)                | LIRB technical data sheet   |   |
|   | C/S T.007, 5(g)                | Electrical diagramme of the LIRB battery pack                                     |   |
|   | C/S IP(LIRB) Appendix C        | Description of Beacon Charger, its working cycle and indication                   |   |
|   | C/S IP(LIRB) 2.5               | Pre-test discharge analysis, in the format of Table A-C.1                         |   |
|   | C/S IP(LIRB) 3.3.2             | Estimation of reversible and irreversible capacity loss during TBRC (test report) |   |
|   | C/S IP(LIRB) 3.3.3 (i)         | Estimation of Irreversible Capacity Loss during Storage (test report)             |   |
|   | C/S IP(LIRB) 3.3.3 (ii)        | Estimation of Irreversible Capacity Loss during Stand-by Mode (test report)       |   |
|   | C/S IP(LIRB) 3.5               | Estimation of the Worst Case Life Time? WCLT (test report)                        |   |
|   | C/S IP(LIRB) 3.6.2             | Beacon Charger test report  |   |
|   | C/S IP(LIRB) 3.1.5             | Indiction of WCLT in the User Manual  |   |
|   | C/S IP(LIRB) 3.2               | Description of the battery charge indication in the User Manual                   |   |
|   | C/S IP (LIRB) 1.6              | Beacon labels and markings (indication of TBRC and battery replacement date)      |   |
|   | C/S IP (LIRB) 3.6.1            | Confirmation that the charger is compliant with national safety/EMC requirements  |   |

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(date)

(beacon model)

(beacon manufacturer's point of contact for the type approval: name, job title, e-mail address)

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(signature)

## APPENDIX C TO ATTACHMENT A

Table A-C.1: Pre-Test LIRB Discharge Calculation

| Characteristic  | Designation      | Units  | Value | NOTES  |
|---|------------------|--------|-------|--|
| Nominal LIRB capacity (*)   | $C_{BN}$         | mA-hrs |       | (*) in the column “Characteristic” indicates that this parameter is declared by the beacon manufacturer                  |
| Time between recommended charges, TBRC (*)                                  | TBRC             | days   |       |  |
| Worst case life time, WCLT (*)  | WCLT             | days   |       | Check, that:<br>(WCLT -1 month) > TBRC   |
| Battery storage time, prior to battery installation in the beacon (*)       | STC              | years  |       |  |
| Beacon storage time (*)   | STB              | years  |       |  |
| Total storage time  | STT              | years  |       | $STT = STC + STB$  |
| Maximum storage time  | STM              | years  |       | If $STT < 2$ yrs, $STM = 2$ yrs<br>If $STT \geq 2$ yrs, $STM = STT$  |
| Rate of irreversible storage losses during 2-year maximum storage time (*)  | LIRR-STM-%       | %      |       |  |
| <b>Irreversible capacity loss during storage</b>                            |                  |        |       |  |
| Battery replacement period (*)  | BRP              | years  |       |  |
| Rate of irreversible capacity loss during battery replacement period (*)    | LIRR-BRP-%       | %      |       |  |
| <b>Irreversible capacity loss during battery replacement period</b>         |                  |        |       |  |
| Average stand-by current (**)   | ISB              | mA     |       | (**) in the column “Characteristic” indicates the outcome of verification tests by the test facility                     |
| Rate of Reversible capacity loss during TBRC(**)                            | LREV-TBRC-%      | %      |       |  |
| <b>Reversible capacity loss during TBRC</b>                                 |                  |        |       |  |
| Rate of Irreversible capacity loss during TBRC(**)                          | LIRREV-TBRC-%    | %      |       | (**)   |
| <b>Irreversible capacity loss during TBRC</b>                               |                  |        |       |  |
| Number of self-tests during battery replacement period(*)                   | N <sub>ST</sub>  |        |       |  |
| Average self-test current (**)  | I <sub>ST</sub>  | mA     |       |  |
| Self-test duration (**)   | T <sub>ST</sub>  | sec    |       |  |
| <b>Capacity loss due to self-tests</b>                                      |                  |        |       |  |
| Maximum number of GNSS self-tests during battery replacement period (*)(**) | N <sub>GST</sub> |        |       |  |
| Average GNSS self-test current (**)   | I <sub>GST</sub> | mA     |       |  |
| Maximum GNSS Self-test duration (**)  | T <sub>GST</sub> | sec    |       |  |
| <b>Capacity loss due to GNSS self-tests</b>                                 |                  |        |       |  |
| Other Capacity Losses   | L <sub>OTH</sub> | mA-hrs |       |  |
| Calculated value of the battery pack pre-test discharge                     | C <sub>DC</sub>  | mA-hrs |       | $C_{DC} = 1.65 * (LIRR-STM + LIRR-BRP + LREV-TBRC + LIRREV-TBRC + LST + LGST + LOTH)$<br>See section 3.1 for definitions |